

NON-AXISYMMETRIC EFFECTS ON LONG LIQUID BRIDGES

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Abstract—The stability of long liquid bridges under non-axisymmetric disturbances like a micro-gravitational force acting perpendicular to the liquid bridge axis or a non-coaxiality of the disks is analyzed through an asymptotic method based on bifurcation techniques. Results obtained indicate that such non-axisymmetric effects are of higher order than those produced by axisymmetric perturbations.

1. INTRODUCTION

In the last 10 years, a significant number of theoretical and experimental papers dealing with the behavior of liquid bridges in a low gravity environment have been published. Such studies are interesting because a liquid bridge is, under a strictly mechanical point of view, similar to the fluid configuration appearing in the crystal growth process known as the floating zone technique. In most of these papers (a short review of the literature in this field can be found in Meseguer and Sanz[1]) only axisymmetric liquid bridges under axisymmetric perturbations are considered, and only in a few of them non-axisymmetric effects like the C-mode[2,3] or gravitational forces acting perpendicular to the liquid bridge axis[4,5] have been treated.

In each one of the two European missions of Spacelab (Spacelab-1 and Spacelab-D1) an experiment dealing with the stability of long liquid bridges under mechanical disturbances has been performed. One of the problems arising in the analysis of such experimental results is that experimental configurations were not exactly those foreseen because of a disalignment of the axes of the disks supporting the liquid column (Spacelab-1)[6]. The question to be answered is how this disalignment modifies the stability of the liquid bridge.

Theoretical analysis and experiments performed on Earth seem to indicate that non-axisymmetric perturbations are less important than axisymmetric ones. For example, Coriell *et al.*[4] stated that the effect of a transversal microgravity on the stability limit of a slender liquid bridge is of the order of the square of the perturbation, whereas the effects produced by axisymmetric perturbations like small volume changes, axial microgravity or a small difference in disks diameter are of the order of the perturbation in the first case and of the order of the two-thirds power of the perturbation in the second two[7].

In this paper, the stability of long liquid bridges under non-axisymmetric perturbations is analyzed by using an asymptotic method based on the idea of the bifurcation equation, already used in the case of isorotating liquid bridges by Vega and Perales[3]. This method simplifies the calculation of the equilibrium shapes (either stable or unstable) and stability limits, allowing the knowledge of the character of the branching points (sub- or supercritical).

The main result here obtained is that non-axisymmetric perturbations have a negligible effect on stability limit when compared with axisymmetric ones. An additional consequence of the analysis here presented is that, in most cases, the study of the symmetries appearing in the problem is sufficient to establish the order of the modification of the maximum stable length of a liquid bridge under a given perturbation, without solving the whole problem.

2. PROBLEM FORMULATION

Let us consider a slender liquid bridge as sketched in Fig. 1: a liquid column held by surface tension forces between two circular disks of radius R_0 placed a distance L apart. Both disks are parallel but non-coaxial, $2E$ being the distance between both axes. The liquid bridge is subject to a transversal gravity g and its volume is equal to that of a cylindrical column held between two coaxial disks of radius R_0 at a distance L ($V = \pi R_0^2 L$).

Let $R = R(Z, \theta)$ the equation of the liquid bridge interface. If the fluid is at rest the equation governing the interface shape is obtained by expressing the equilibrium between the different pressure forces at the interface

$$\sigma (1/R_1 + 1/R_2) + P_0 - P_a + \rho g R \cos(\theta + \alpha) = 0, \quad (1)$$

where α is the angle between the plane defined by the axes of the disks and the direction of transversal microgravity, g the acceleration due to this gravity, σ the surface tension, R_1 and R_2 the principal radii of curvature, ρ the liquid density, P_a the ambient pres-

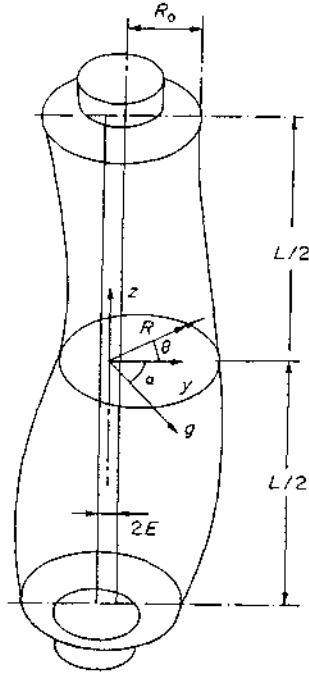


Fig. 1. Geometry and coordinate system for the perturbed liquid bridge.

sure and P_0 a yet unknown constant giving the origin of pressures inside the liquid bridge. To calculate P_0 the condition that the volume of the liquid bridge remains equal to that of a cylinder must be imposed, that is

$$\int_{-L/2}^{L/2} dz \int_0^{2\pi} R^2(Z, \theta) d\theta = 2\pi LR_0^2. \quad (2)$$

The boundary conditions are

$$\begin{aligned} R(\pm L/2, \theta) &= \pm E \cos \theta \\ &+ (R_0^2 - E^2 \sin^2 \theta)^{1/2}, \quad R(Z, \theta) = R(Z, \theta + 2\pi), \end{aligned} \quad (3)$$

which state that the liquid bridge remains anchored to the disk edges and has azimuthal periodicity, respectively.

As it will be demonstrated later, within the approximation of our study, the effects on stability limits of the considered non-axisymmetric perturbations (lateral microgravity and axes disalignment) are decoupled, that is, the stability limit variation is independent of α . Therefore, from now on, only the case $\alpha = 0$ will be considered. Observe that this implies that the microgravity direction is on the plane defined by disk axes.

Introducing the following dimensionless variables and parameters

$$\begin{aligned} A &= L/2R_0, \quad E = E/R_0, \quad B = \rho g R_0^2/\sigma, \\ P &= (P_0 - P_a)R_0/\sigma, \\ z &= Z/R_0, \quad F(z, \theta) = R(Z, \theta)/R_0, \end{aligned} \quad (4)$$

where A is the liquid bridge slenderness, E the dimensionless axes separation, B the gravitational

Bond number and P the dimensionless reference pressure, the formulation of the problem becomes

$$M[F] + P + BF \cos \theta = 0, \quad (5)$$

$$\int_{-A}^A dz \int_0^{2\pi} F^2(z, \theta) d\theta = 4\pi A, \quad (6)$$

$$\begin{aligned} F(\pm A, \theta) &= \pm E \cos \theta + (1 - E^2 \sin^2 \theta)^{1/2}, \\ F(z, \theta) &= F(z, \theta + 2\pi), \end{aligned} \quad (7)$$

$M[F]$ being the dimensionless local mean curvature, $M[F] = R_0(1/R_1 + 1/R_2)$, which can be expressed as [8]

$$\begin{aligned} M[F] &= [F(1 + F_z^2)(F_{\theta\theta} - F) + FF_{zz}(F^2 + F_\theta^2) \\ &- 2F_\theta(F_\theta + FF_z F_{\theta z})][F^2(1 + F_z^2) + F_\theta^2]^{-3/2}. \end{aligned} \quad (8)$$

3. CRITICAL POINTS

Critical points are given by the solution of the linear problem. Since in the base $B = 0$, $E = 0$ the system (5)–(7) has the trivial solution $F = 1$, $P = 1$, let us expand these variables in the form

$$\begin{aligned} F(z, \theta) &= 1 + \epsilon f(z, \theta) + O(\epsilon^2), \\ P &= 1 + \epsilon p + O(\epsilon^2), \end{aligned} \quad (9)$$

where $\epsilon \ll 1$ is a small parameter standing for the interface deformation.

After substituting these expressions in the system (5)–(7) the following linear problem results

$$f + f_{zz} + f_{\theta\theta} + p = 0, \quad (10)$$

$$\int_{-A}^A dz \int_0^{2\pi} f(z, \theta) d\theta = 0, \quad (11)$$

$$f(\pm A, \theta) = 0, \quad f(z, \theta) = f(z, \theta + 2\pi). \quad (12)$$

As it is well-known[9] all solutions to this problem are axisymmetric, the expression of the interface depending on A . For $A = k\pi$ ($k = 1, 2, \dots$) the interface shape results

$$f(z, \theta) = \sin\left(\frac{k\pi z}{A}\right), \quad p = 0, \quad (13)$$

whereas the case $A = A_k$ (where A_k satisfies $A_k - \tan A_k = 0$) yields

$$f(z, \theta) = -p \left(1 - \frac{\cos z}{\cos A}\right). \quad (14)$$

For $B \rightarrow 0$, $E \rightarrow 0$ the bifurcation to non-cylindrical equilibrium shapes (although axisymmetric) appears only near $A = k\pi$ or $A = A_k$ (Implicit Function Theorem [10]). Nevertheless, only the bifurcation near $A = \pi$, which is the smallest value of A , is significant in practice because this point represents the transition from stable to unstable shapes. The following bifurcation points cannot be reached because the liquid bridge will break before.

Therefore, in the case $B = 0$, $E = 0$, the instability

appears at $A = \pi$ and the unstable equilibrium shapes are defined by

$$f(z, \theta) = \sin z, \quad p = 0. \quad (15)$$

In conclusion, eqn (15) is the solution that must be perturbed to calculate the variation of the maximum stable slenderness when non-axisymmetric effects like transversal microgravity or non-coaxiality of the disks are present ($B \neq 0$, $E \neq 0$).

4. BIFURCATION EQUATION

Since non-axisymmetric effects decrease the slenderness at which the liquid bridge becomes unstable, let us introduce, as in Rivas and Meseguer[11] a new parameter λ measuring the slenderness decrease due to the effect of transversal microgravity or disks offset, and a new variable x which normalizes boundary conditions

$$\lambda = \frac{\pi - A}{\pi}, \quad x = \frac{z}{1 - \lambda}. \quad (16)$$

To calculate the variation of the critical slenderness with B and E a standard bifurcation technique can be used[3], retaining higher order terms than those in the linear problem. Let $g(x, \theta)$ and q the expressions representing these higher order terms in the expressions of the interface shape and pressure, respectively. Then, by taking into account expressions (15) the interface shape and pressure can be written as

$$F(x, \theta) = 1 + \epsilon \sin x + g(x, \theta), \quad P = 1 + q. \quad (17)$$

Therefore, after substituting expressions (16) and (17) in eqns (5)–(7) the problem formulation becomes

$$M[1 + \epsilon \sin x + g(x, \theta)] + 1 + q + B[1 + \epsilon \sin x + g(x, \theta)] \cos \theta = 0, \quad (18)$$

$$\int_{-\pi}^{\pi} dx \int_0^{2\pi} [1 + \epsilon \sin x + g(x, \theta)]^2 d\theta = 4\pi^2, \quad (19)$$

$$g(x, \theta) = g(x, \theta + 2\pi),$$

$$g(\pm \pi, \theta) = \pm E \cos \theta + (1 - E^2 \sin^2 \theta)^{1/2} - 1 = \pm E \cos \theta - \frac{1}{2} E^2 \sin^2 \theta + \dots \quad (20)$$

One additional condition must be added to unique define the parameter ϵ ,

$$\int_{-\pi}^{\pi} dx \int_0^{2\pi} g(x, \theta) \sin x d\theta = 0; \quad (21)$$

observe that this condition defines ϵ as

$$\epsilon = \frac{\int_{-\pi}^{\pi} dx \int_0^{2\pi} F(x, \theta) \sin x d\theta}{\int_{-\pi}^{\pi} dx \int_0^{2\pi} \sin^2 x d\theta}. \quad (22)$$

The problem (18)–(21) provides ϵ , $g(x, \theta)$ and q in terms of B , E and λ . As $B \rightarrow 0$, $E \rightarrow 0$ such functions can be calculated by means of standard perturbation

techniques[12,13]. However, a direct use of this techniques requires anticipation of certain properties of the solution. This may be avoided by using the idea of the bifurcation equation[14,3]. Instead of eqn (18) let us consider the following equation

$$M[1 + \epsilon \sin x + g(x, \theta)] + 1 + q + B[1 + \epsilon \sin x + g(x, \theta)] \cos \theta + \phi \sin x = 0. \quad (23)$$

The Implicit Function Theorem[10] shows that expressions (19)–(21) and (23) uniquely define

$$\phi = \phi(\epsilon, B, E, \lambda),$$

$$g = g(x, \theta; \epsilon, B, E, \lambda), \quad p = p(\epsilon, B, E, \lambda), \quad (24)$$

at least when ϵ , B , E , and λ are sufficiently small.

Such solutions correspond to the solution of eqns (18)–(21) if and only if ϵ , B , E and λ satisfy

$$\phi(\epsilon, B, E, \lambda) = 0, \quad (25)$$

which is called the bifurcation equation [observe that, in this case, eqn (23) is identical to eqn (18)].

5. BIFURCATION ORDER

Before solving the problem (19)–(21) and (23) a study of the symmetries involved in the problem will allow us to anticipate some characteristics of the solution. Therefore, since the problem is invariant under the following set of symmetries

$$x \rightarrow -x, \quad \epsilon \rightarrow -\epsilon, \quad E \rightarrow -E, \quad \phi \rightarrow -\phi, \quad (26)$$

$$x \rightarrow -x, \quad \theta \rightarrow \theta + \pi, \quad \epsilon \rightarrow -\epsilon,$$

$$B \rightarrow -B, \quad \phi \rightarrow -\phi, \quad (27)$$

$$\theta \rightarrow \theta + \pi, \quad B \rightarrow -B, \quad E \rightarrow -E, \quad (28)$$

and its solution is unique, the function ϕ must satisfy

$$\phi(\epsilon, B, E, \lambda) = -\phi(-\epsilon, B, -E, \lambda), \quad (29)$$

$$\phi(\epsilon, B, E, \lambda) = -\phi(-\epsilon, -B, E, \lambda), \quad (30)$$

$$\phi(\epsilon, B, E, \lambda) = \phi(\epsilon, -B, -E, \lambda). \quad (31)$$

For the sake of clarity, from now on only the two simple cases $B = 0$, $E \neq 0$ and $B \neq 0$, $E = 0$ will be considered. Let us assume $\phi(\epsilon, B, E, \lambda)$, $g(x, \theta; \epsilon, B, E, \lambda)$ and $q(\epsilon, B, E, \lambda)$ to be expanded as

$$\phi(\epsilon, B, E, \lambda) = \sum_{\substack{i,j=1 \\ k,l=1}}^{\infty} \epsilon^i B^j E^k \lambda^l \phi_{ijkl},$$

$$g(x, \theta; \epsilon, B, E, \lambda) = \sum_{\substack{i,j=1 \\ k,l=1}}^{\infty} \epsilon^i B^j E^k \lambda^l g_{ijkl}(x, \theta), \quad (32)$$

$$q(\epsilon, B, E, \lambda) = \sum_{\substack{i,j=1 \\ k,l=1}}^{\infty} \epsilon^i B^j E^k \lambda^l q_{ijkl}.$$

Then, concerning $\phi(\epsilon, B, E, \lambda)$, its Taylor expansion can be simplified taking into account eqns

(29)–(31). Therefore, in the case $B = 0$, $E \neq 0$ [eqns (29) and (30)] such Taylor expansion will be

$$\begin{aligned} \phi(\epsilon, 0, E, \lambda) &= \epsilon \phi_1(\epsilon^2, E^2, \lambda) \\ &= \phi_{3000}\epsilon^3 + \phi_{1020}\epsilon E^2 + \phi_{1001}\epsilon \lambda + \dots, \end{aligned} \quad (33)$$

whereas the case $B \neq 0$, $E = 0$ [eqns (30) and (31)] yields

$$\begin{aligned} \phi(\epsilon, B, 0, \lambda) &= \epsilon \phi_2(\epsilon^2, B^2, \lambda) \\ &= \phi_{3000}\epsilon^3 + \phi_{1200}\epsilon B^2 + \phi_{1001}\epsilon \lambda + \dots \end{aligned} \quad (34)$$

Therefore, setting $\phi = 0$, eqns (33) and (34) give the slenderness decrease λ as a function of the interface deformation ϵ , the non-axisymmetric perturbation E or B , respectively, and the corresponding coefficients ϕ_{ijkl} . For instance, in the case $B = 0$, $E \neq 0$ such expression will be

$$\lambda = -(\phi_{3000}/\phi_{1001})\epsilon^2 - (\phi_{1020}/\phi_{1001})E^2 + \dots \quad (35)$$

This expression has been represented in Fig. 2. Since the maximum stable slenderness is reached when $\epsilon = 0$, it can be concluded that critical slenderness should vary in the form

$$\lambda_c = -(\phi_{1020}/\phi_{1001})E^2 - (\phi_{1200}/\phi_{1001})B^2 + \dots \quad (36)$$

Observe that, since non-axisymmetric effects decrease the critical slenderness both coefficients, ϕ_{1020}/ϕ_{1001} and ϕ_{1200}/ϕ_{1001} , must be negative.

6. RESULTS AND CONCLUSIONS

When Taylor expansions (32) are introduced into eqns (19)–(21) and (23) and the coefficient of each monomial $\epsilon^i B^j E^k \lambda^l$ is set to zero, a recursive sequence of linear problems results, which allow calculation of ϕ_{ijkl} , q_{ijkl} and $g_{ijkl}(x, \theta)$. Then, the following results are obtained

$$\begin{aligned} g_{1000}(x, \theta) &= \sin x, \\ g_{2000}(x, \theta) &= -\frac{1}{4} + \frac{1}{4} \cos 2x, \\ g_{0001}(x, \theta) &= 0, \end{aligned}$$

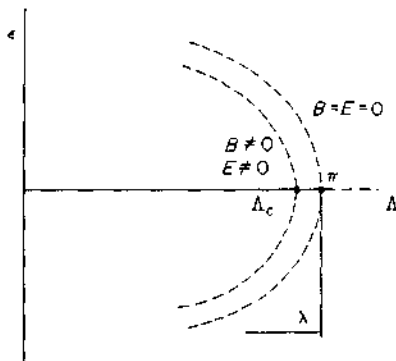


Fig. 2. Bifurcation diagram. Liquid bridge deformation ϵ vs slenderness λ . This plot shows the influence of the dimensionless transversal microgravity B or disk offset E in the bifurcation.

$$g_{0010}(x, \theta) = \frac{x}{\pi} \cos \theta,$$

$$g_{1010}(x, \theta) = \frac{1}{\pi} \cos \theta (1 + \cos x),$$

$$\begin{aligned} g_{0020}(x, \theta) &= \frac{1}{4\pi^2} \cos 2\theta \left(x^2 + 1 - \frac{\cosh \sqrt{3}x}{\cosh \sqrt{3}\pi} \right) \\ &\quad - \frac{1}{4\pi^2} x^2, \end{aligned}$$

$$g_{0100}(x, \theta) = \frac{1}{2}(\pi^2 - x^2) \cos \theta,$$

$$g_{1100}(x, \theta) = -(x \cos x + x - 3 \sin x) \cos \theta,$$

$$\begin{aligned} g_{0200}(x, \theta) &= -\frac{1}{16}(\pi^2 - x^2)^2 + \frac{1}{2}(x^2 + \pi^2 \cos x) \\ &\quad - \frac{\pi^2}{4}(1 + \cos x) + \left[\frac{1}{16}(\pi^2 - x^2)^2 \right. \end{aligned}$$

$$\left. + \frac{1}{6} \left(1 - \frac{\cosh \sqrt{3}x}{\cosh \sqrt{3}\pi} \right) \right]$$

$$\left. + \frac{3}{4} \left(x^2 - \pi^2 \frac{\cosh \sqrt{3}x}{\cosh \sqrt{3}\pi} \right) \right] \cos 2\theta; \quad (37)$$

$$\phi_{1000} = \phi_{2000} = \phi_{0001} = \phi_{0002} = \phi_{0010} = \phi_{1010} = 0,$$

$$\phi_{0011} = \phi_{0020} = \phi_{0100} = \phi_{0101} = \phi_{1100} = \phi_{0200} = 0,$$

$$\phi_{3000} = -\frac{3}{2}, \quad \phi_{1001} = 2,$$

$$\phi_{1020} = -\frac{3}{2\pi^2}, \quad \phi_{1200} = -\frac{\pi^2}{2}, \quad (38)$$

where most of these coefficients have been directly canceled, as resulting from the symmetries analysis presented in Section 5. Therefore, according to expressions (38) when non-axisymmetric effects are considered the critical slenderness decreases in the form

$$\lambda_c = \frac{3}{4\pi^2} E^2 + \frac{\pi^2}{4} B^2 + \dots, \quad (39)$$

which coincides with the result obtained by Coriell *et al.* [4] in the case $B \neq 0$, $E = 0$.

An important characteristic to be pointed out is that the results here obtained do not depend on the angle between the plane defined by the axes of the disks and the direction of transversal microgravity (see Fig. 1), so that eqn (39) remains the same although this angle was not equal to zero. In consequence, it must be noted that there is no coupling between the two considered non-axisymmetric perturbations, that is, the term of order BE is equal to zero.

In conclusion, it has been demonstrated that, in the two cases analyzed, branching is subcritical, and that a cylindrical long liquid bridge will be stable when its slenderness is smaller than the critical slenderness

$$\lambda_c = \pi \left(1 - \frac{3}{4\pi^2} E^2 - \frac{\pi^2}{4} B^2 + \dots \right). \quad (40)$$

On the other hand, the expression for the stable equilibrium shapes is

$$F(x, \theta) = 1 + E g_{0010}(x, \theta) + E^2 g_{0020}(x, \theta) + B g_{0100}(x, \theta) + B^2 g_{0200}(x, \theta) + \dots \quad (41)$$

where the functions g_{ijk} are given by the expressions (37).

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