

# **Acoustic effects on the free oscillations of the top membrane of a cylindrical container**

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# Objectives

Calculate the natural frequencies of the top membrane of a cylindrical container filled with a compressible and inviscid fluid

# Introduction

Fluid-structure interaction problems  
many technological applications  
known for many years

Most works concerned underwater  
applications,  
nuclear reactor, naval engineering

# Applications – Fluid-Membrane

## \* Microelectromechanical systems MEMS

Micropumps

Ultrasonic transducers

Pressure sensors

Performance this microsystems

Controlling resonant frequency

reducing power requirements (micropumps)

resonant frequency-fluid pressure (pressure sensors)

## \* Liquid containers (nuclear reactor, aerospace vehicles )

Interesting to know the frequencies of the coupled system

Liquid frequencies can be close to other frequencies of the system resulting in a disturbance of the motion and even instability and failure

A shifting of these frequencies is a way of remedy the problem

This is done by covering the free liquid surface with a flexible structural member, such as a membrane or a thin elastic plate

- \* Pressure accumulators (hydraulic systems)
  - elastic cover separates fluid domains
  - prevent system instabilities

## Other applications

- \* Sonar

fluid effects on vibration elastic cover of a cavity

- \* Biological prosthesis

Smart structures (membranes), low mass

Influence fluid low density important

# Existing Methods (fluid-containers elastic membrane)

Variational formulation

Kinetic (plate + fluid) + Potential Energy

Application

incompressible  
inviscid

## Authors (problem studied)

Bauer

Cylindrical rectangular containers

Tariverdilo

Cylindrical container

## Deformation modes

Vaccum modes      Bessel, Harmonic - functions

## Present Method

Wave equation - Velocity potential - Separation of variables  
Pressure field - Bernoulli's linearized equation  
Integration dynamic equation - frequencies

## Aplication

Compressible, inviscid fluid  
all modes

## Problem formulation

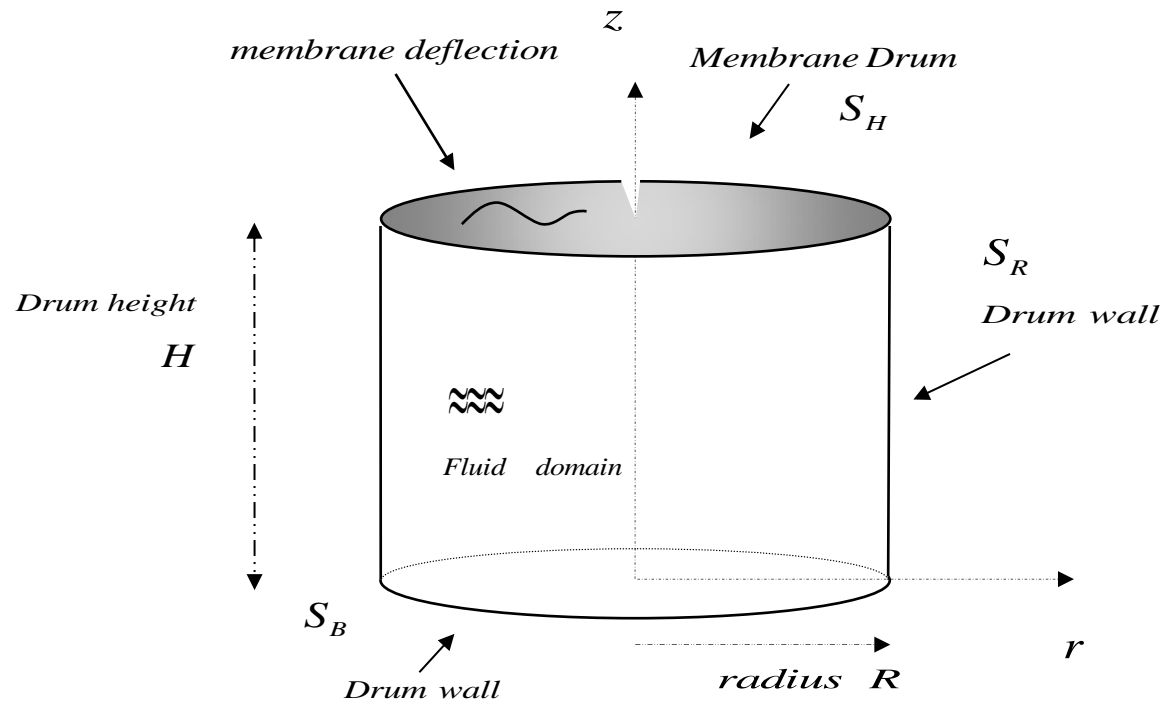
The deformation equation

$$T\Delta\eta(r, \theta, t) - \rho_m t_h \frac{\partial^2 \eta}{\partial t^2} = p(r, \theta, H, t)$$

Fluid-membrane boundary condition  $z = H$

$$\frac{\partial p}{\partial z} = -\rho_f \cdot \frac{\partial^2 \eta}{\partial t^2}$$

Fig. 1. Scheme of the cylindrical container with the top membrane showing the different geometrical parameters



# Harmonic motion, frequency $\omega$

(separation variables)

$$\eta(r, \theta, t) = \tilde{\eta}(r, \theta) \cdot e^{i\omega t}$$

$$\varphi(r, \theta, z, t) = \tilde{\varphi}(r, \theta, z) \cdot e^{i\omega t}$$

## Membrane deformation

$$\eta(r, \theta, t) = \sum_{m,n} \eta_m^n(r, \theta) \cdot \bar{d}_m^n \cdot e^{i\omega_m^n t}$$

## Vacuum modes

$$\eta_m^n(r, \theta) = J_m(\beta_m^n r) \cdot \cos(m\theta)$$

Modal parameters  $m, n$  interger values

Number nodal circles  $n$  zero deformation

nodal diameters  $m$

## Deformation parameter

$$d_m^n(t) = \bar{d}_m^n \cdot e^{i\omega_m^n \cdot t}$$

Deformation weight coefficient  $\bar{d}_m^n$

## Deformation of the membrane

$$\eta(r, \theta, t) = \sum_{m,n} \eta_m^n(r, \theta) \cdot \bar{d}_m^n \cdot e^{i\omega_m^n t}$$

Bessel function  $m$  order  $J_m(\beta_m^n r)$

Parameter  $\beta_m^n$  roots of equation  $J_m(\beta_m^n R) = 0$

Vaccum Frequency  $\beta_m^n = \omega_{mv}^n \sqrt{\frac{\rho_m t_h}{T}}$

# Fluid- Velocity Potential $\varphi$ (compressible, inviscid fluid)

Wave equation (Helmholtz)  $\Delta\varphi - \frac{1}{c^2} \frac{\partial^2 \varphi}{\partial t^2} = 0$

Fluid velocity field

$$\vec{v}_f = \nabla \varphi$$

$$\Delta\tilde{\varphi} + k^2\tilde{\varphi} = 0$$

## Boundary conditions

wave number  $k = \frac{\omega}{c}$

Rigid walls  $\frac{\partial \varphi}{\partial n} = 0$

Membrane  $\frac{\partial \varphi}{\partial z} = \frac{\partial \eta}{\partial t}$   $z = H$

# Solution of the Potential

## Separation of variables

Being  $\alpha_m^n$  the roots of

And the parameter  $\lambda_m^n = \sqrt{(\alpha_m^n)^2 - k^2}$

$$\dot{\alpha}_m^n(t) = i \cdot \omega_m^n \cdot \alpha_m^n(t) = i \cdot \omega_m^n \cdot \bar{\alpha}_m^n \cdot e^{i \cdot \omega_m^n \cdot t}$$

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## Applying Boundary Condition over Membrane, after integration

$$\frac{\partial \varphi}{\partial z} = \frac{\partial \eta}{\partial t}$$

Expanding in series, after integration of squared integrands

## Orthogonality properties

## Momentum's linearized equation

$$\frac{\partial \varphi}{\partial t} + \frac{p}{\rho_f} = 0$$

## Pressure over membrane

$$\ddot{d}_m^n(t) = \frac{d^2(d_m^n(t))}{dt^2} = -\omega_m^{n2} \cdot \bar{d}_m^n \cdot e^{i \cdot \omega_m^n \cdot t}$$

# Harmonic motion - Pressure jump over membrane

$$p(r, \theta, t) = \sum_{m,n} P_m^n(r, \theta) \bar{d}_m^n e^{i\omega_m^n t}$$

Pressure mode,  $P_m^n(r, \theta)$

$$P_m^n(r, \theta) = \frac{\rho_f \coth(\lambda_m^n H)}{\lambda_m^n} \sqrt{\frac{\Lambda_{\beta m}^n}{\Lambda_{\alpha m}^n}} \varphi_m^n(r, \theta) \omega_m^{n2}$$

# Integration of squared dynamic equation

(orthogonality condition)

## Frequency equation

$$A_m^n \cdot \omega_m^{n 4} + B_m^n \cdot \omega_m^{n 2} + C_m^n = 0$$

## Coefficients

$$A_m^n = \left[ \frac{\rho_f \coth(\lambda_m^n H)}{\lambda_m^n} \right]^2 - (\rho_m t_h)^2$$

$$B_m^n = 2\rho_m t_h T \beta_m^{n^2}$$

$$C_m^n = -T^2 \beta_m^{n^4}$$

Iteration procedure ,  $\lambda_m^n(k)$  wave number  $k$

$$\lambda_m^n = \sqrt{(\alpha_m^n)^2 - k^2}$$

## Fluid mass parameter

Multiplying the membrane equation expanded in series by the deformation mode  $\eta_u^v(r, \theta)$ , and after integration over the membrane circular surface

With orthogonality properties, and making the sum in  $u, v$  indices, the following formula for natural frequency is obtained for each value of indices  $m, n$

$$\omega_m^n = \sqrt{\frac{K_m^n}{M_m^n + M_{Fm}^n}}$$

$$K_m^n = \pi \cdot \Lambda_{\beta m}^n \cdot T \cdot (\beta_m^n R)^2$$

$$M_m^n = \pi \cdot \Lambda_{\beta m}^n \cdot \rho_m \cdot t_h \cdot R^2$$

$$M_{Fm}^n = \pi \frac{\rho_f \coth(\lambda_m^n H)}{\lambda_m^n} \sqrt{\frac{\Lambda_{\beta m}^n}{\Lambda_{\alpha m}^n}} R^2 \cdot \sum_i \frac{\beta_m^i R}{(\beta_m^i R)^2 - (\alpha_m^n R)^2} J_m(\alpha_m^n R) (J_{m-1}(\beta_m^i R) - J_{m+1}(\beta_m^i R))$$

And the Fluid mass parameter

$$C_{MF_m^n} = \frac{M_{Fm}^n}{\rho_f \pi R^2 H}$$

## Results

Table 1 Natural frequencies (Hz) for the membrane of the cylindrical drum (in vacuum and water) for the present method and the work of Tariverdilo et al. [13], of radius  $R=60$  mm, drum height  $H=60$  mm and membrane thickness  $t_h=0.5$  mm

$m,n$	$f_v$	$f_i$ (Tarverdilo)	$f_i$ (present method)	Relative discrepancy (%)
0,0	54.9	--	15.4	
0,1	46.5	--	46.5	
0,2	85.3	--	85.3	
0,3	123.3	--	123.3	
1,0	87.5	19.2	17.0	11.4
1,1	160.1	52.9	52.4	0.95
1,2	232	94.6	93.2	1.48
1,3	304	159	138.9	12.6
2,0	117	32.7	29.6	2.77
2,1	192	70.8	69.6	1.69
2,2	265	115.7	113.5	1.90
2,3	337	185.9	161.5	1.31
3,0	145	46.7	43	7.92
3,1	222	88.9	87	2.13
3,2	297	136.8	134	2.05
3,3	370	212.8	184	13.5
4,0	173	61.2	57	6.86
4,1	252	107.3	105	2.14
4,2	328	157.9	155	1.84
4,3	402	239.5	207	13.5

# Membrane -Cylindrical Container - Properties

Container Height  $H = 2 \text{ m}$

Fluid density  $\rho_f = 1,225 \frac{\text{kg}}{\text{m}^3}$

Radius  $R = 1 \text{ m}$

Membrane Thickness  $t_h = 0,02 \text{ mm}$

Frequency parameter  $\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$

Membrane Material  $\rho_m = 2700 \frac{\text{kg}}{\text{m}^3}$

Membrane Tension  $T = 100 \frac{\text{N}}{\text{m}}$

Fig. 2 Variation of the frequency parameter with the radius of the membrane for different modes, n=0,1,2 nodal circles and zero nodal diameter m=0

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

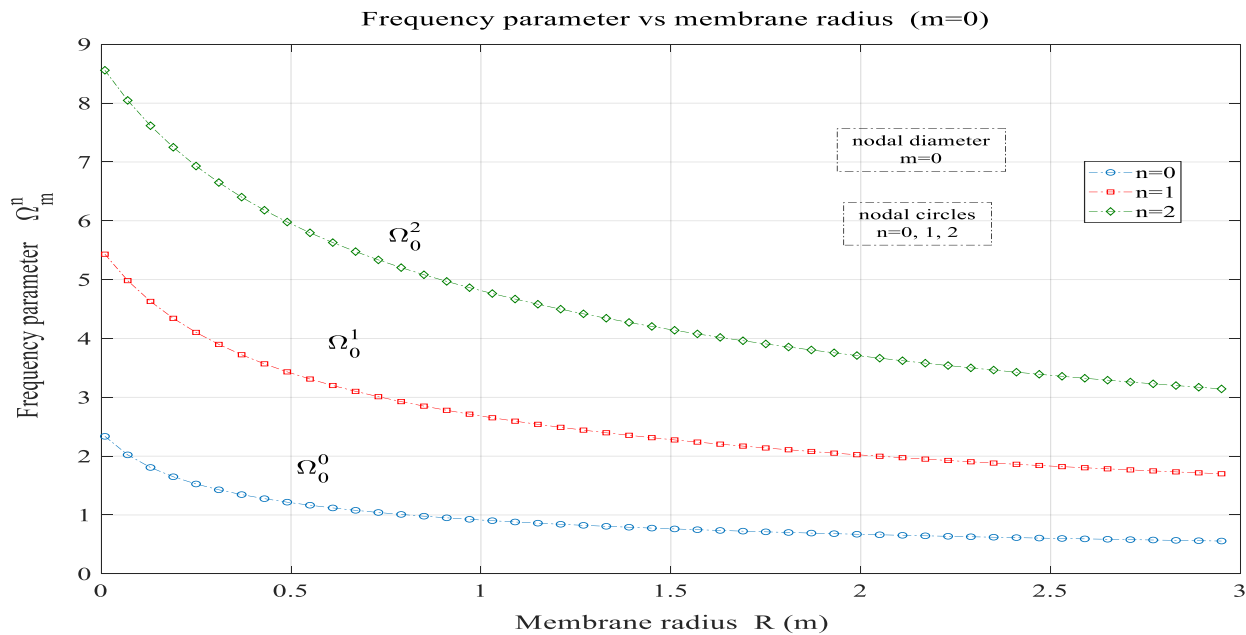
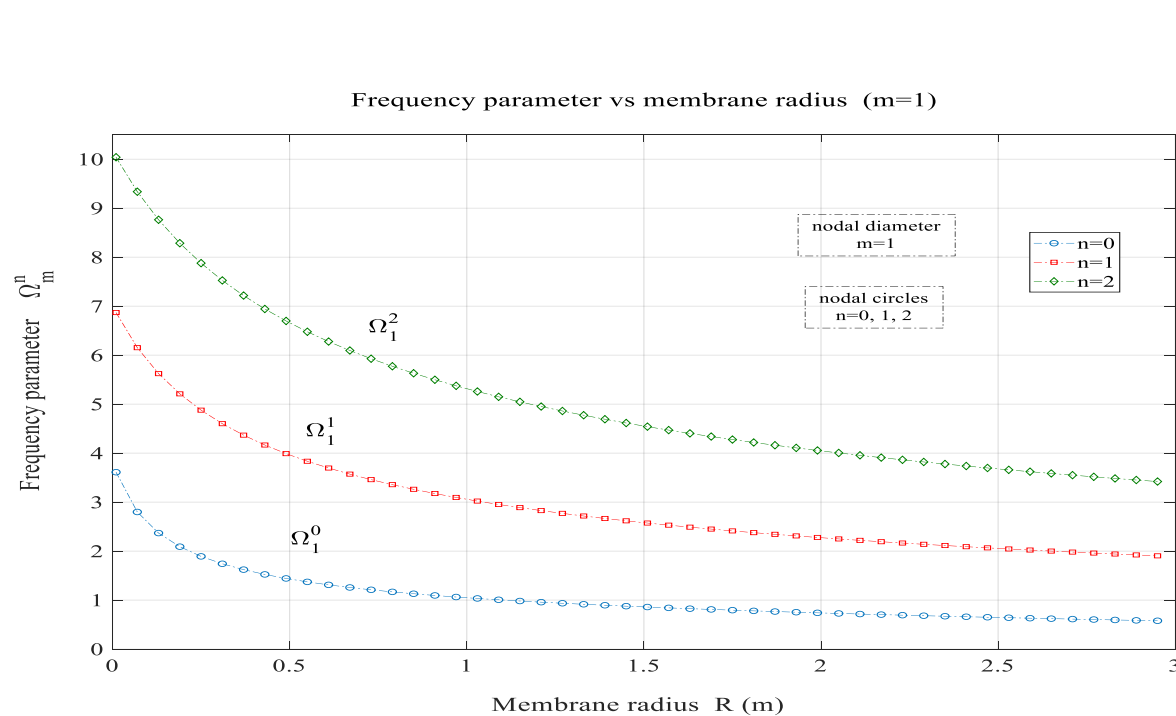
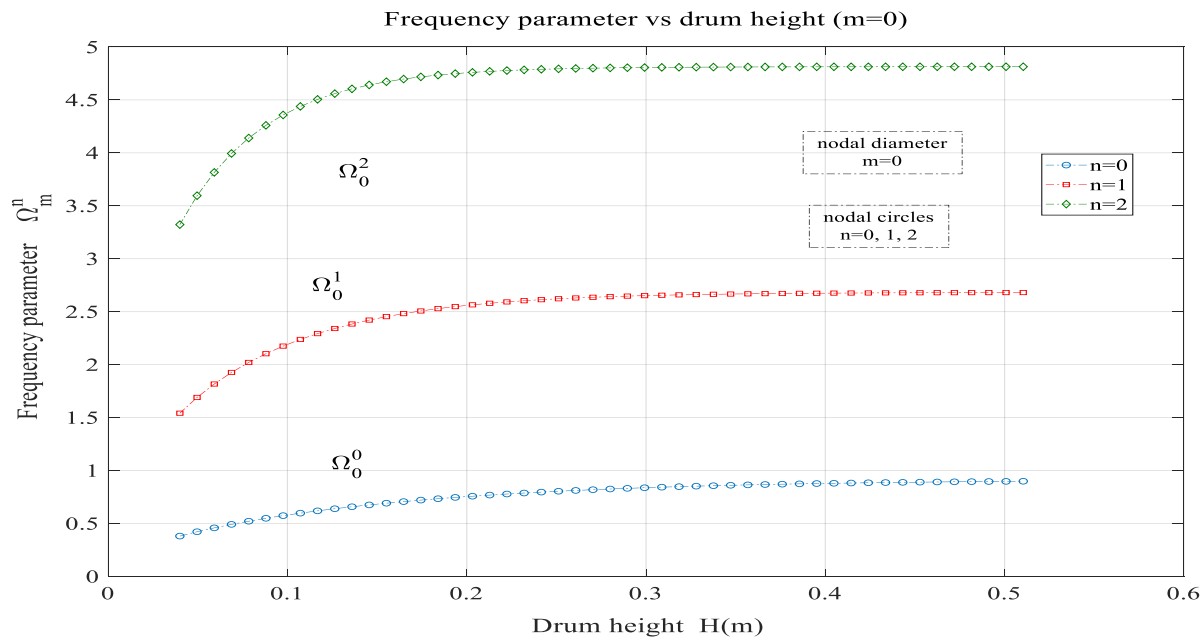


Fig. 3 Variation of the frequency parameter with the radius of the membrane for different modes,  $n=0,1,2$  nodal circles and one nodal diameter  $m=1$



$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

Fig. 4 Variation of the frequency parameter with the drum height H for different modes, n=0,1,2 nodal circles and zero nodal diameter m=0



$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

Fig. 5 Variation of the frequency parameter with the drum height H for different modes, n=0,1,2 nodal circles and one nodal diameter m=1

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

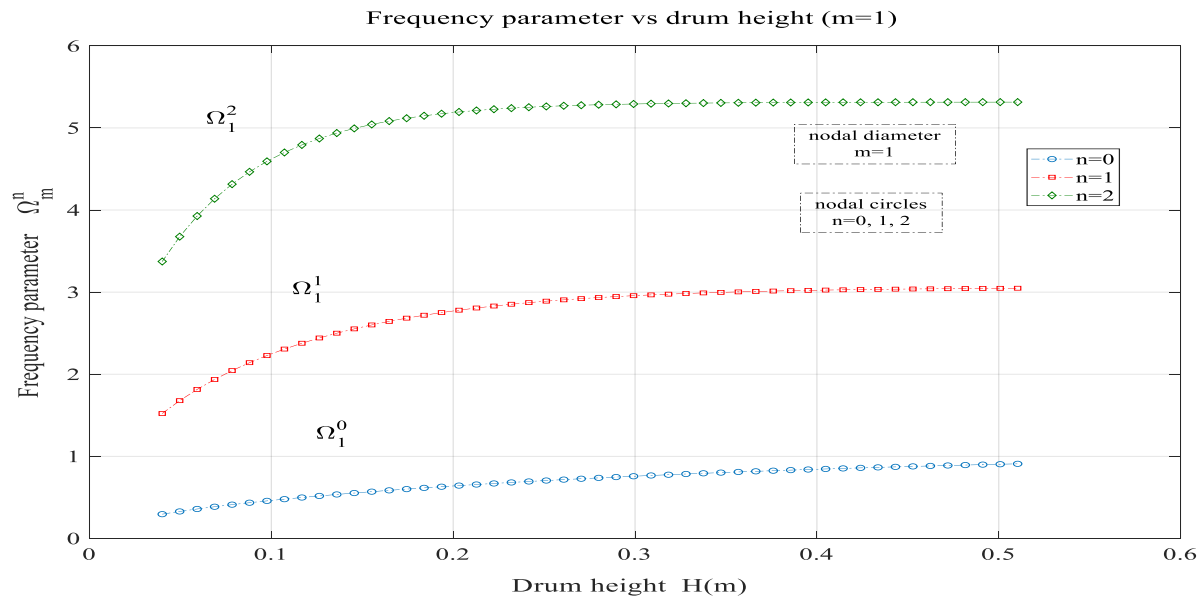
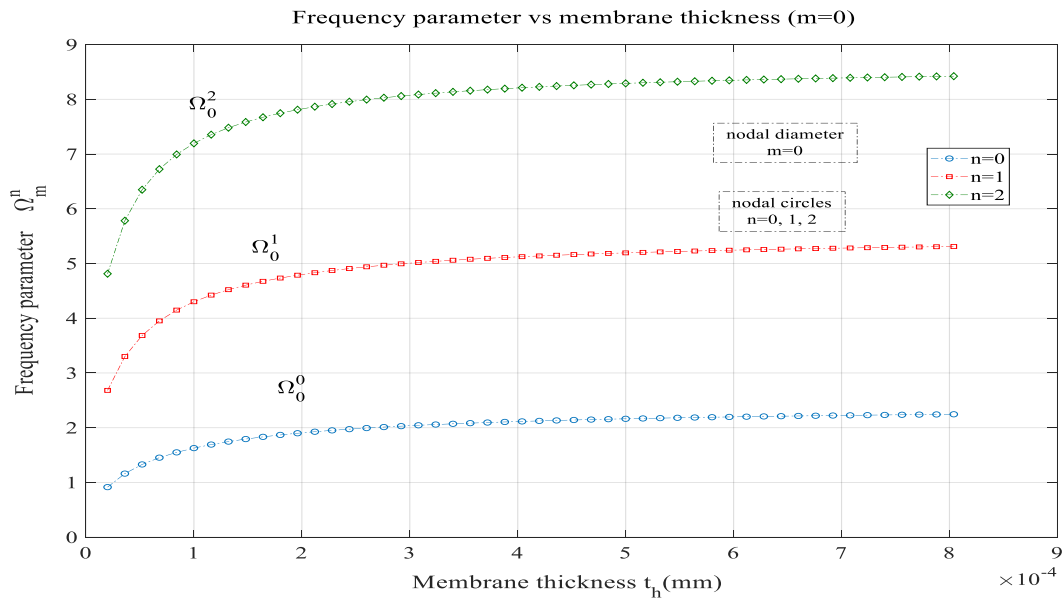


Fig. 6 Variation of the frequency parameter with the membrane thickness for different modes,  $n=0,1,2$  nodal circles and zero nodal diameter  $m=0$



$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

Fig. 7 Variation of the frequency parameter  $\Omega$  with the membrane thickness for different modes,  $n=0,1,2$  nodal circles and one nodal diameter  $m=1$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

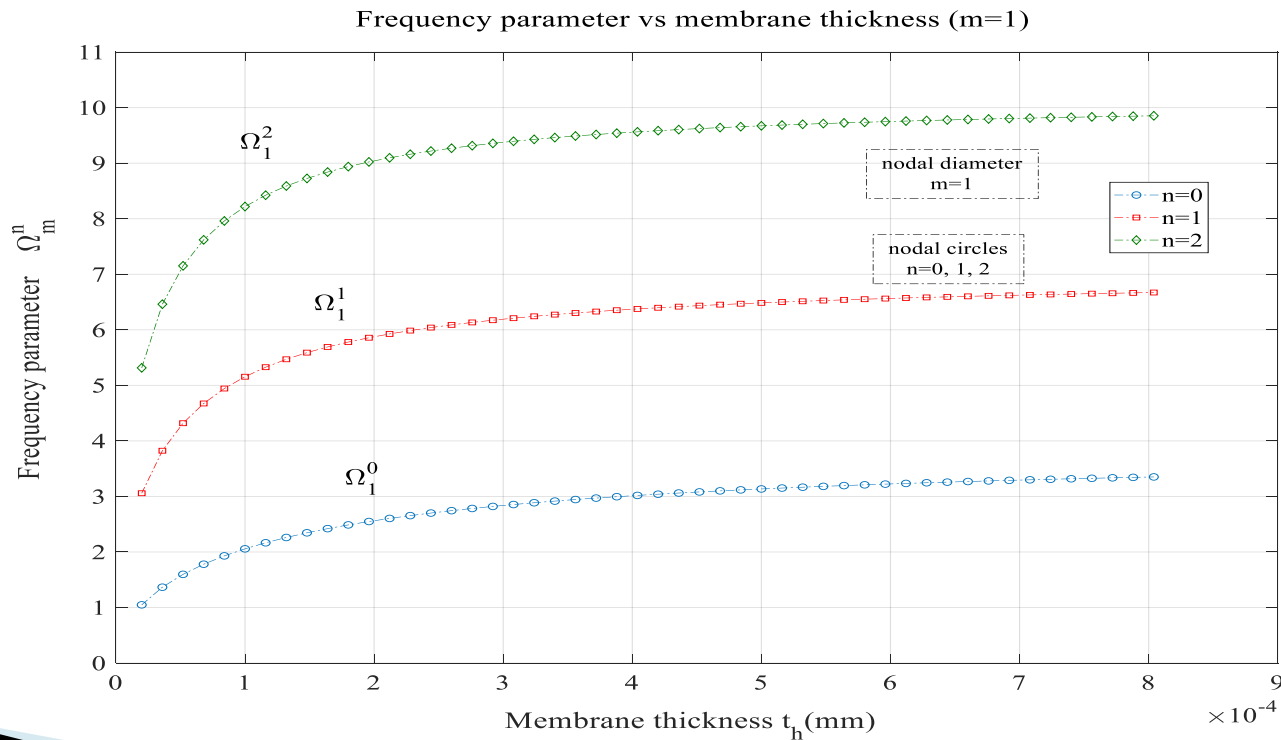


Fig. 8 Variation of the frequency parameter with the fluid density for different modes,  $n=0,1,2$  nodal circles and zero nodal diameter  $m=0$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

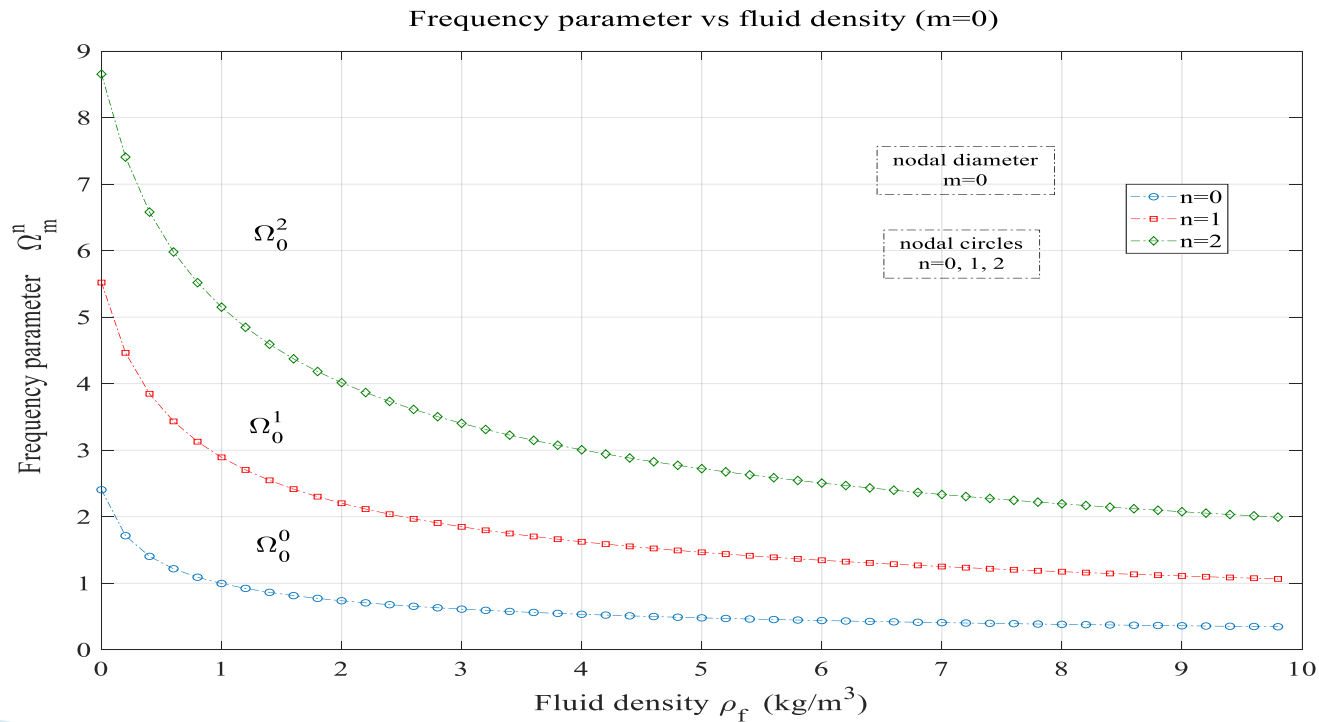


Fig. 9 Variation of the frequency parameter with the fluid density for different modes,  $n=0,1,2$  nodal circles and one nodal diameter  $m=1$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

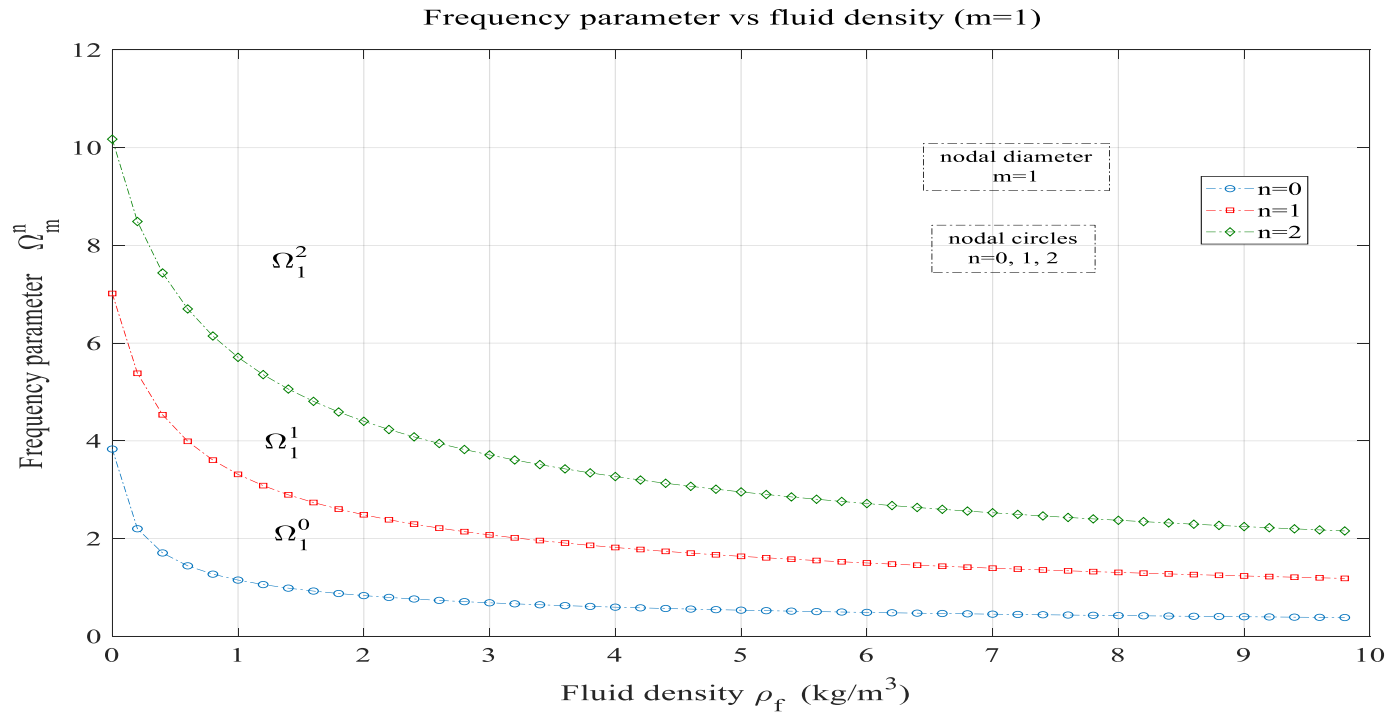


Fig. 10 Variation of the frequency parameter with the membrane material density for different modes,  $n=0,1,2$  nodal circles and zero nodal diameter  $m=0$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

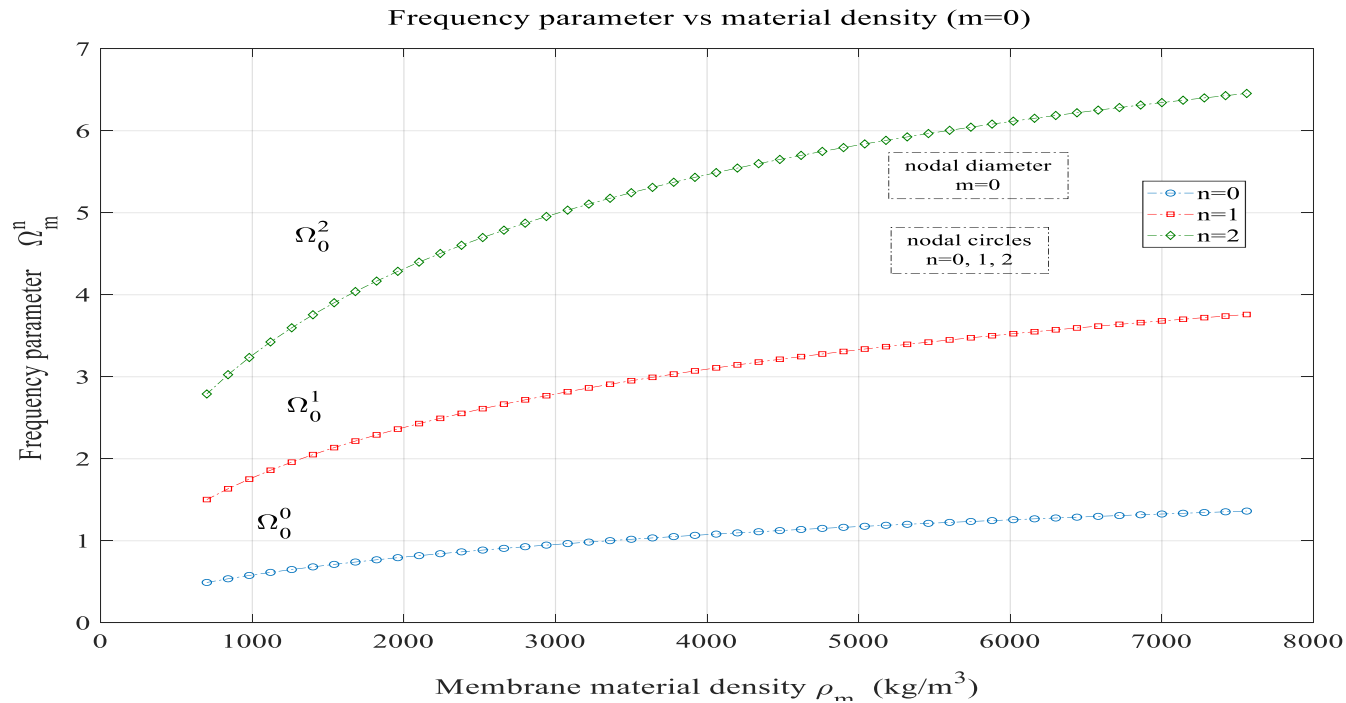


Fig. 11 Variation of the frequency parameter with the membrane material density for different modes,  $n=0,1,2$  nodal circles and one nodal diameter  $m=1$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

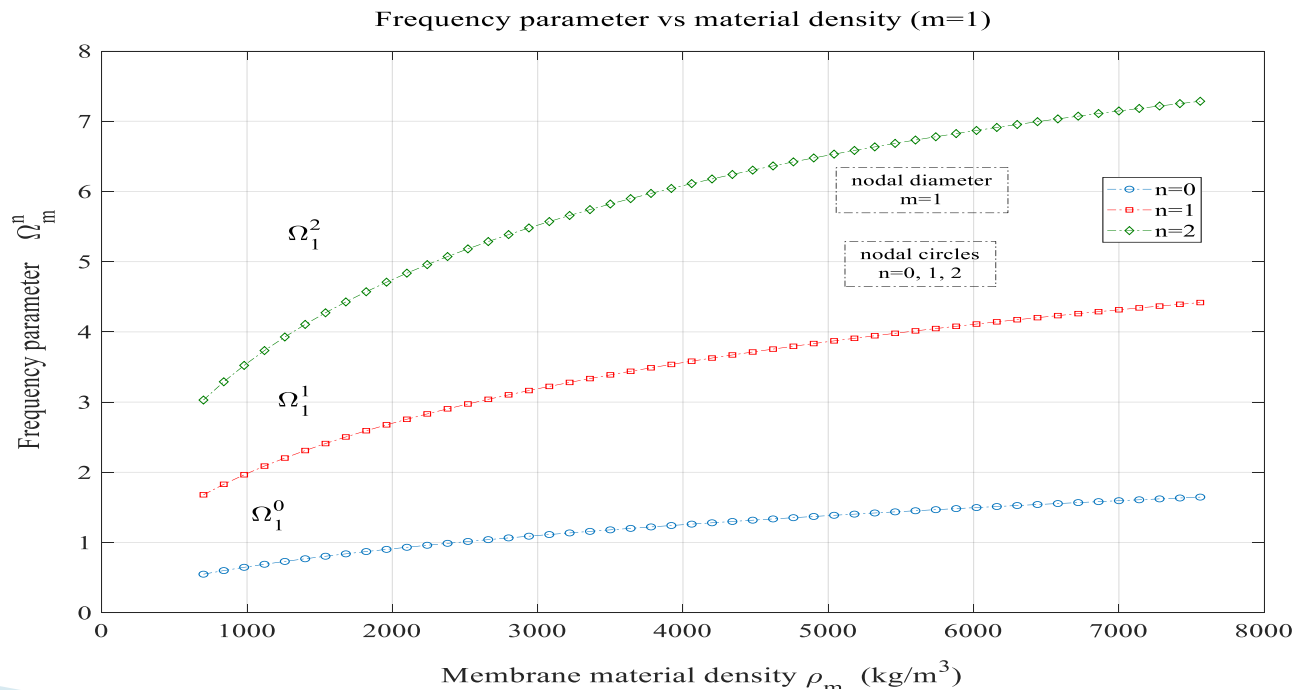


Fig. 12 Variation of the frequency parameter with the fluid sound speed for different modes,  $n=0,1,2$  nodal circles and zero nodal diameter  $m=0$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

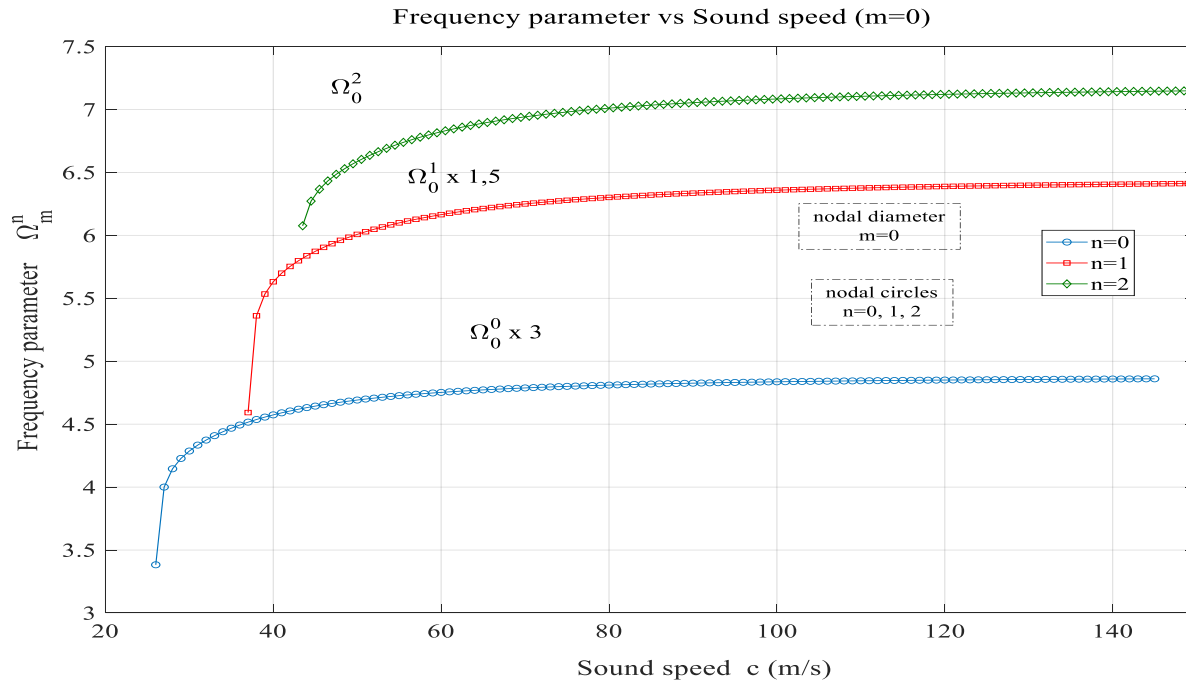


Fig. 13 Variation of the frequency parameter with the fluid sound speed for different modes,  $n=0,1,2$  nodal circles and one nodal diameter  $m=1$

$$\Omega = \sqrt{\frac{\rho_m t_h}{T}} R \cdot \omega$$

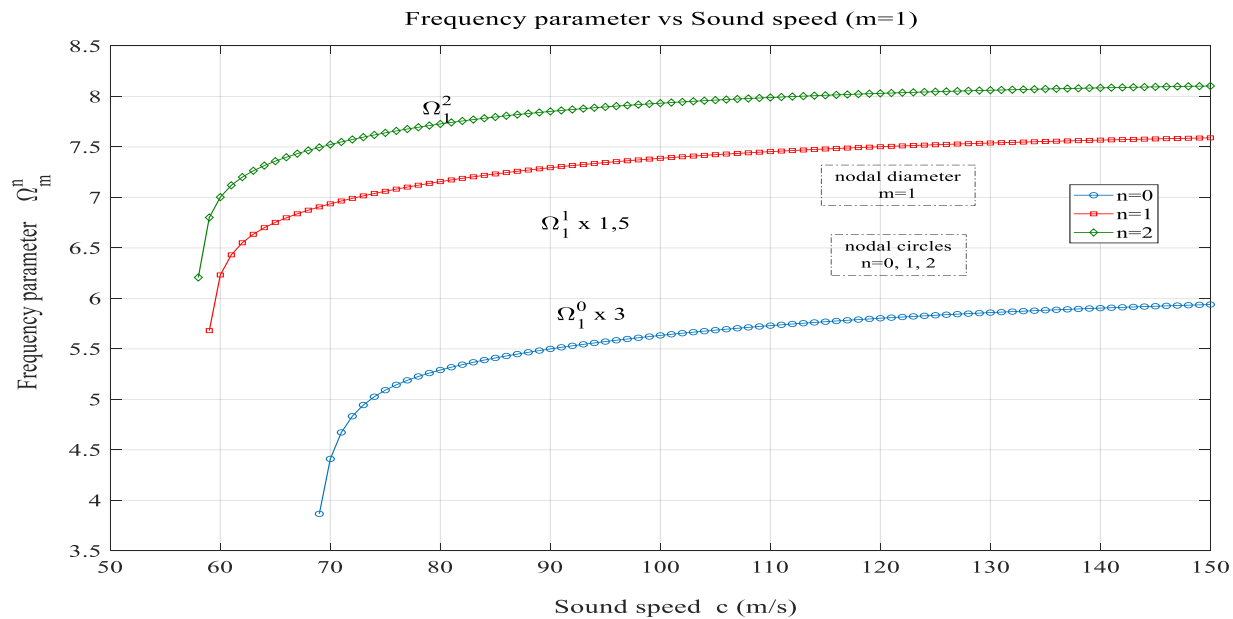


Fig. 14 Variation of the fluid mass parameter with the excitation frequency for the mode  $m = 0$  and  $n = 0$

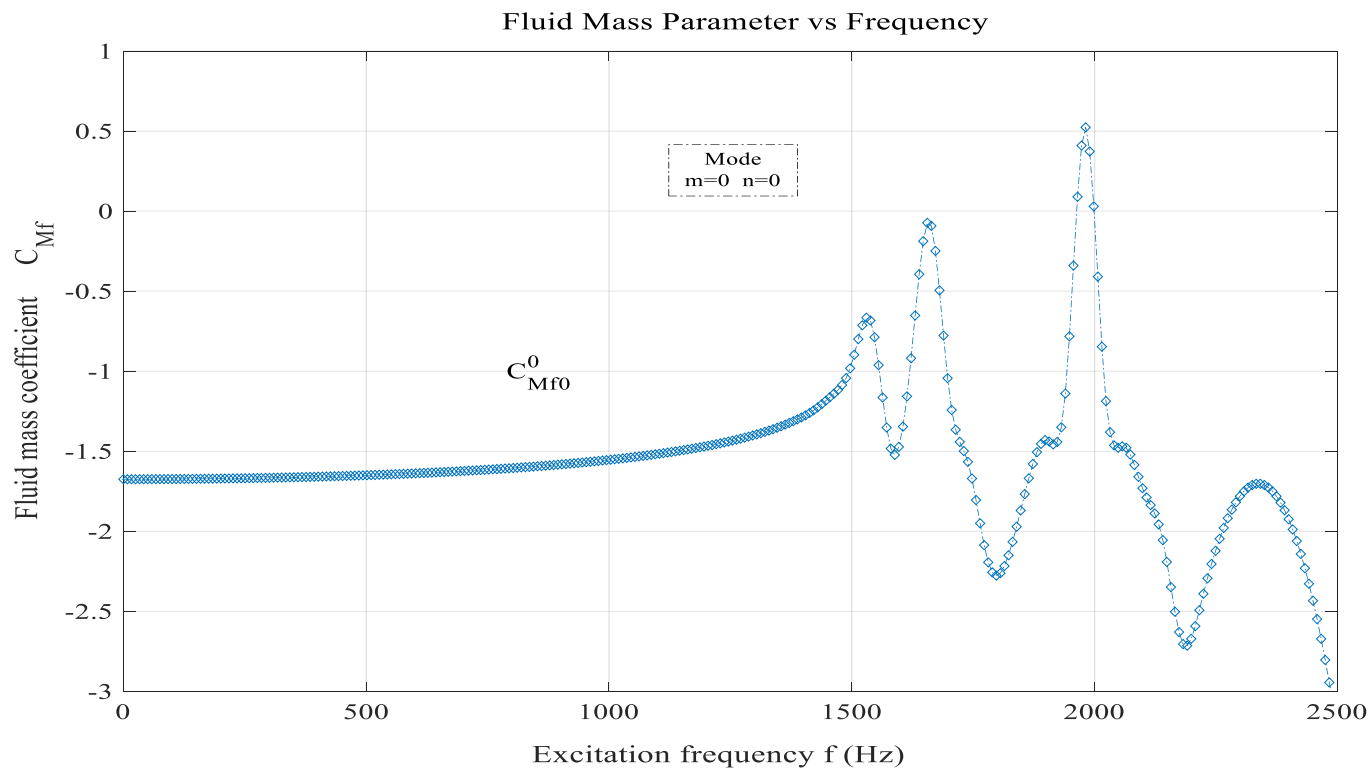


Fig. 13 Variation of the fluid mass parameter with the excitation frequency for the mode  $m = 1$  and  $n = 0$

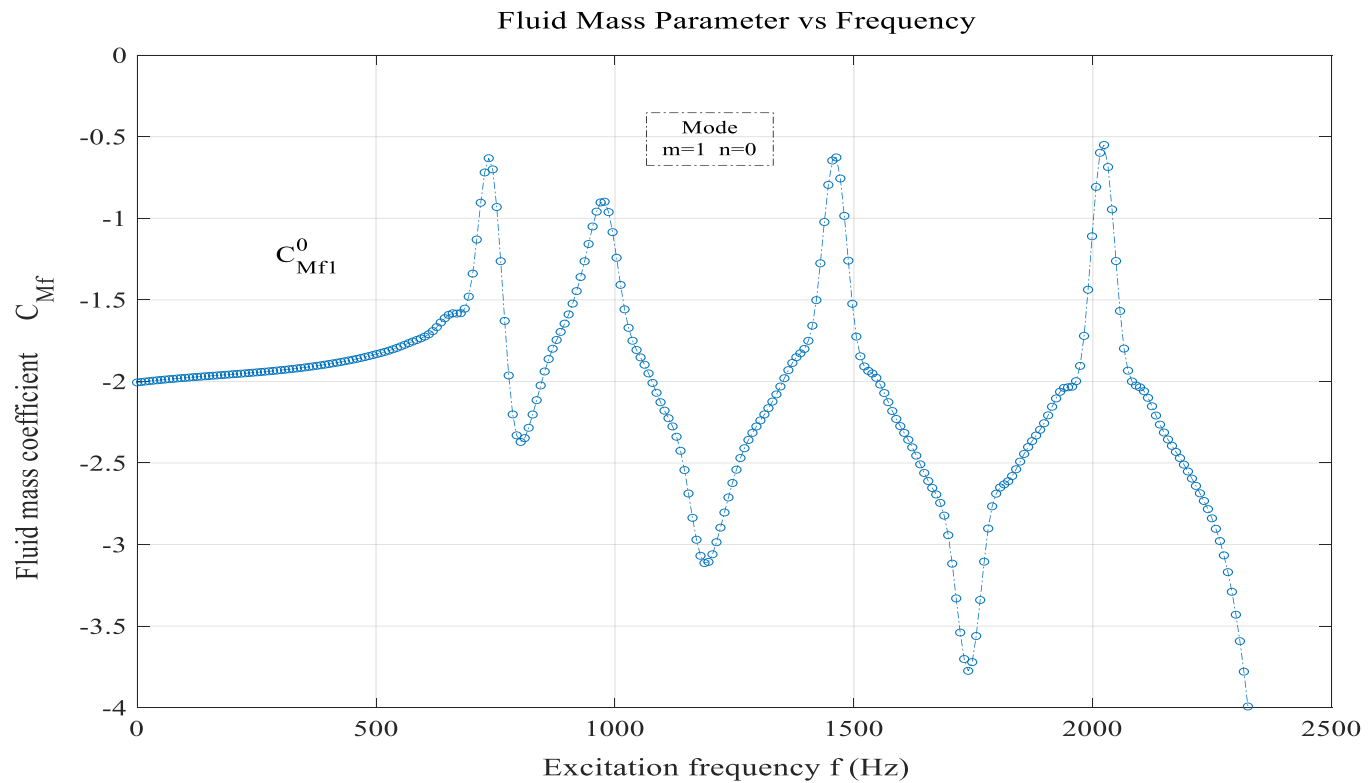


Table 2. Natural frequencies (Hz ) for the aluminum membrane of a cylindrical container filled with fluid (air density) and in the vacuum case for different modes, with radius  $R = 1 m$  , container height  $H = 2 m$  and membrane thickness  $t_h = 0,02 mm$

$m , n$	$f_v$	$f_a$	Frequency reduction (%)
0 , 0	16.47	6.26	62.0
0 , 1	37.81	18.37	51.4
0 , 2	59.27	32.96	44.4
0 , 3	80.76	49.10	39.2
1 , 0	26.24	7.18	72.6
1 , 1	48.05	20.94	56.4
1 , 2	69.68	36.40	47.8
1 , 3	91.26	53.19	41.7

## Conclusions

Method calculate frequency top membrane of  
cylindrical container filled compressible inviscid fluid

Wave equation - Fluid velocity Potential - Separation  
variables

Momentum's Linearized equation - Pressure field

## Dynamic equation integration – membrane coupled frequencies

Frequency parameter Variation: –Radius, Drum Height, Sound speed, Membrane Thickness, Material density, and Fluid density

Fluid mass parameter frequency Spectrum

Validation other methods